

PID Controller Parameters Tuning Based on Pole Assignment Optimal Prediction for Power Station Boiler Superheated Steam Temperature

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ABSTRACT:

In view of the long-time delay and large inertia of boilersuperheatedsteamtemperaturecontrol, thispaperproposedaself-tuningcontrolstrategybasedonPoleAssignmentOptimalPrediction. ModelparametersareidentifiedbyLeast squares algorithm with forgetting factor, andthenaccordingtotheestimationmodelofsuperheatedsteam temperature object, the PID parameters are tuned bydesigning the adaptive law with the method of Pole AssignmentOptimal Prediction. Consequently the closed-loop system hasdesired characteristics; also this control strategy can solve theproblemofthelong-timedelayofboilersuperheated steamtemperature. Finallythesimulationresultshaveshownthemethod has good dynamic and static control performances forthiscomplicatedsuperheatedsteamtemperaturecontrolsystem, and meet the actual superheated steam temperature controlrequirements.

Index Terms—Poleassignment,optimalprediction,forgetting factor, PID parameters tuning, superheated steamtemperature.

INTRODUCTION

PIDcontroliswidelyusedinindustry,forlargernonlinearsystems the parameters of control object often need to betuned at different working points, and the tuning process isnot easy, so the versatility is not strong for different objects. Fuzzycontrol[1],[2]andneuralcontrol[3],[4]fornonlinearsystemcanachievebettercontroleffect, buttheestablishment of fuzzy rules and the application of neuralnetworkmodelarestillbuiltinthebasisofexperience, anditis difficult to obtain the specific description of closed-loopcontrol characteristics.

The pole placement algorithm is a commonly used designmethodwithintuitivelydesignandgoddynamicperformance, which can adapt to the unstable inverse system(non-minimumphasesystem)andopen-loopunstable system. The method of pole placement based on input-output transferfunction model is one of the mature control methods amongthemoderncontroltheories. Itcanimplementsspecifiedclosedloopcharacteristicsfor linear time-invariant objectandfurther improve thedynamic response and robustness.

Forlargedelayobject,Smith[5]firstlyproposedapredictivecontrollerwhichcouldimprovethecontrolquality. Palmer[6]andWatanabe[7]pointedoutthedefectsinthe practicalapplications,thuslimitingitsapplication. Keyser[8]proposedself-

tuningpredictivecontroller,especiallytheapplicationsofself-tuningpredictivePIDcontrollerweregiven, butitsdrawbackisthatthecontrolparameterswerealsochosenbyexperience. Thispaperproposedapoleassignmentoptimalpredictionself-

tuningPIDcontrollerwhichcombinedonlineidentificationofthemodelparametersandtheonlinedesignofthecontroller . Theparameteridentificationusedrecursiveleast squaresalgorithm with forgetting factor, while the controller adoptedpoleassignmentopticalpredictionalgorithm. Themethodnotonlyachievedthedesiredcontrolcharacteristics, andforlarge delay problem of the superheated steam temperature butalso obtained goodcontrol quality.

The superheated steam temperature of high temperaturesuperheater for power station boiler was one of the maincontrolparametersofthethermalcontrolsystem. ThecontrolsystemmainlyadoptedconventioncascadePIDcontrol. Underseriousinterferenceandvariedworkingcondition,itiscdifficult to achieve ideal control effect. Hence a lot of newcontrol strategies which combined predictive control methodand the traditional PID control appeared [9]-

[12]. In this paper, the outer PID parameters tuning adopted the pole assignment optimal prediction algorithm, and combined the inner PID controller to control the superheated steam temperature.

The main research contents of the paper include the following three aspects. Firstly, aiming at the problem of model parameter estimation, we adopt the least squares algorithm with forgetting factor. It can effectively identify the parameters of superheated steam temperature. Secondly, aiming at the superheated steam temperature control system of Power Station Boiler, a cascade compound control strategy that combines an outer loop PID master controller adjusted with pole assignment optimal prediction algorithm and an inner loop PID auxiliary controller is adopted. Lastly, the simulation of this method is given in this passage. The result shows that the proposed method can achieve good static and dynamic performances.

I. THE PID CONTROLLER

A. The Continuous PID Controller

In a continuous control system, the PID controller can be expressed as

$$\frac{u(t) - K_p e(t)}{t} = \frac{\frac{e(t)dt}{T_d}}{de(t)} \quad (1)$$

—

(1)

$$\frac{T}{dt} \quad (1)$$

0

dt

Use Laplace transform, so it can be written in transfer function form
 $C(z^{-1})$ is weighted polynomial of the disturbance object.

$$u(s) = \frac{1}{A(z^{-1})} \cdot \frac{1}{z^{n_a}}$$

$$= K_p \frac{1 - Ts}{1 + \frac{Ts}{T_d}}$$

$$(2) \quad \frac{1}{e(s)} = \frac{(n)}{p} \quad \frac{d}{z^{n_b}}$$

$$= \frac{Ts}{1 - \frac{Ts}{T_d}}$$

$$= \frac{B(z^{-1})}{B(z^{-1})} \cdot \frac{b}{bz^{-1}}$$

$$= z^{-n_b} \cdot b$$

$$= 0$$

$$I = 0 \quad 1 \quad (n) \quad 0$$

—

$$C(z^{-1}) = 1 - cz^{-1} - \dots - c_z^{-n_c}$$

B. The Discrete PID Controller

In a digital system, in order to realize PID control, the continuous PID controller should be converted to discrete PID controller. If the sampling period is T_0 , the discrete PID controller uses difference equation to express as

where,

$$= 1 \quad (n)$$

$$a = [a, a, \dots, a, b, b, \dots, b]^T$$

$$\frac{1}{P} \frac{T - \sum_0^k}{T}$$

$$e(k) = e(k-1)$$

$$d = \frac{T}{T} [y(k-1), y(k-2), \dots, y(k-n), u(k-d), u(k-d-1), \dots, u(k-d-n)]$$

$$u(k) = K$$

$$(e(k))$$

$$I = I = 0$$

$$Te(k-i) = T$$

$$)$$

$$0$$

$$(3)$$

$$b$$

This can be written in vector form

Transform(3) by Z-translation
 $y(k) = C(z^{-1})e(k)$
 (7)

$$u(z) = K_P$$

$$(e(z)) = T_0$$

$$T_I$$

$$\frac{1}{1 - z^{-1}}$$

$$e(z)$$

(4)

The observation vector T and the estimation parameter vector were substituted into the recursive least squares
 $\boxed{T_d(e(z) - z^{-1}e(z))T_0}$

The discrete pulse transfer function formulas. So the parameters of the controlled object could be identified online.

With forgetting factor recursive least squares algorithm formula can be expressed as

$$\boxed{\frac{0}{z^{-1}}} \frac{r_0 z^{-1} r z^{-2}}{1 - \frac{P(k-1) - (k)}{2}} = \frac{P(k-1) - (k)}{2}$$

$$\boxed{\frac{K(k)}{e(z)}} = \frac{T P(k-1) - (k)}{1 - z^{-1}}$$

$$\boxed{(k) - (k-1) - K(k)[y(k) - (K) - (K-1)]}$$

where,
 $r_0 = K_P(1 - T_f/T_D/T)$

$$\boxed{P(k) = [1 - K(k)(k)]P(k-1)}$$

- $r \square K(\{ \square 2T/T\})$
- $KT/T \{ r_2 \}^P_D$
- α is the forgetting factor. Its value is selected between 0.95 \square 1 by considering the time-varying parameters,

II. THE DESIGN OF THE LEAST SQUARES ALGORITHM PARAMETER ESTIMATOR

There are a lot of different model parameter identification algorithms, and the least squares algorithm is the most widely used identification algorithm in industrial control because of small online computation and high stability. With the growth of data, the data saturation of ordinary least squares will appear, and with a large amount of calculations, it will lead to a decline in the control of the system. In order to overcome this phenomenon, the recursive least square method with forgetting factor was adopted for the estimation of superheated temperature outer PID controller [13], [14]. The controlled object with Controlled Auto Regressive Moving Average (CARMA) model is expressed as disturbances and the order of the model. K is the gain vector. P is the estimation error covariance matrix.

III. POLE ASSIGNMENT OPTIMAL PREDICTION SELF-TUNING CONTROL ALGORITHM

For linear system, pole distribution not only has an effect on the stability of the system, but also has a great influence on the system dynamic performance such as rise time, overshoot and oscillation frequency etc. Therefore, as long as choose a feedback control law to make the closed-loop poles in the desired position, the closed-loop system performance will meet the prescribed performance index. This is the pole assignment design method [15]. Also in this passage the optimal prediction method is adopted to solve the delay problem in the process control.

By Diophantine equation

$$C(z^{-1})/A(z^{-1})$$

in the object

$$A(z^{-1})y(k) \square z^{-d}B(z^{-1})u(k) \square C(z^{-1}) \square (k)$$

(6)

model which described in (6) can be decomposed into

$$y(k) \text{ is system output, } u(k) \text{ is control quantity, } \square (k) \text{ is}$$

$$C(z^{-1}) \square$$

$$\square 1 \quad \square d \quad G(z^{-1})$$

the noise, d is the delay time of the system,

$$A(z^{-1})$$

and

$$A(z^{-1})$$

$F(z$

$$\square z$$

$$A(z^{-1})$$

(8)

$$B(z^{-1})$$

is weighted polynomial of the controlled object,
where,

$$\square F(z^{-1}) \square 1 \square f z^{-1} \square \dots \square f z^{-d-1}$$

$$T(z^{-1}) \square 1 \square t z^{-1} \square t z^{-2} \square \dots t z^{-m}$$

(16)

$$\begin{array}{ccc} \square & 1 & d \square 1 \\ 1 & 2 & m \\ \square & (z^{-1})^m g_0 g_1 z^{-1} \cdots g_{n-1} z^{-n+1} & \\ (m \square n \square 2) & & \\ \square G(z) = 0 & 1 \\ n \square 1 & & \end{array}$$

Using (6)and(8), wecanget

$$G(z^{-1}) = \frac{y(k)}{C(z^{-1})}$$

$$B(z^{-1})F(z^{-1})$$

$$\overline{C(z^{-1})}$$

$$u(k)$$

(9)

From(15),wecanseethatthererearenolagsinclosed-loopsystemcharacteristicequation. Sothepoleassignmentoptimalpredictionself-tuningPIDcontrolsystemcan overcome long-time delay.

Solve(15),andthenwecangettheparametersofPID

$$F(z^{-1})e(k|d)$$

$y(k|d)|k$ representestimationvalueatthetimeof
($k|d$)according to output valueoftime.

The problem now is to find optimal prediction
 $y^*(k|d)|k$ in $y(k|d)|k$ to maketheleastprediction controller.

From the above, the pole assignment optimal predictionself-tuningalgorithmiscomposedofsystemparameteridentificationandpoleassignmentoptimalpredictionalgorithm.The steps can besummarized as follows

- Settheinitialvalue;includemodelinitialparameter errorvariance,whichsatisfythefollowingformula

$$E[y(k|d)|y^*(k|d)|k]^2$$

and identification coefficient andPetc.

- Samplingthecurrentcontrolledquantityoutputquantityy(k).

$$u(k)$$

and

$$\square E[y(k|d)|\bar{y}(k|d)|k]^2$$

(10)

- IdentifythemodelparameterA(z^{-1})andB(z^{-1}).
- Using(3), $F(z^{-1})$ and $G(z^{-1})$ canbecalculated.

Using (9)and(10),wecan get

- Using(6),theexpectedoutput $y^*(k|d)|k$ calculated.
canbe

$$* \quad G(z^{-1})$$

- The controller parameter $S(z^{-1})$ and $R(z^{-1})$ can be

$$\frac{y(k-d)|k|}{B(z^{-1})F(z^{-1})} = \frac{C(z^{-1})y(k)}{C(z^{-1})}$$

$u(k)$
(11)
calculated by using (12).

- Using (10), the controlled quantity obtained.

$u(k)$

can be

- $u(k)$
substituted into equation (1),
 $y(k)$
can be

In a digital system, the PID controller algorithm with digital filter is commonly used. So (5) can be written as obtained.

- Return to the second step.

$$u(z^1) = \frac{r^0 r z^1 r z^2}{e(z^{-1})(1 - z^{-1})(1 - sz^{-1})}$$

12)

IV. TEMPERATURE CONTROL SYSTEM OF POWER STATION BOILER SUPERHEATED STEAM

So the controller is designed according to the discrete PID controller (12).

The main steam temperature control of the power station boiler is one of the important parameters which will concern

where,

$$y_r \\ y^*(k-d)|k| R(z^{-1}) S(z^{-1}) u(k)$$

$$S(z^{-1}) = (1 - z^{-1})(1 - sz^{-1}) \\ R(z^{-1}) = r^0 r z^1 r z^2 \\ (13)$$

units safety and economic operation. Commonly control methods are double-loop control system using differential compensation signal and cascade control system using the conventional PID controller. But the controlled object has characteristics of great inertia and long-time delay. For these control methods it is difficult to achieve the best control effect. The actual situations show that although some power

Using(6),(9),(11),(13),thepoleassignmentoptimal predictionself-tuningcontrolsystemoutputcanbewrittenas

$$z^{-1}B(z^{-1})R(z^{-1}) \\ y(k) = \frac{S(z^{-1})A(z^{-1})}{S(z^{-1})A(z^{-1}) + B(z^{-1})R(z^{-1})}y_r(k) \\ (14) \\ R(z^{-1})F(z^{-1})B(z^{-1}) + S(z^{-1})C(z^{-1})$$

station have adopted Distributed Control System (DCS), the control quality of steam temperature is still not very ideal. The steam temperature will deviate from the set value above more than 8°C even when the load changes with only 2% MCR/min rate for some power stations. So often the main steam temperature is often controlled by manual operation. It

$$S(z^{-1})A(z^{-1}) + B(z^{-1})R(z^{-1}) \\ e(k) \\ \text{lead to the steady state temperature range expanded to the}$$

From(14),theclosed-loop system characteristic equation is

scope of $\pm 6^\circ\text{C}$, this will reduce the economic operation of the unit and increase labor intensity of operator.

$$S(z^{-1})A(z^{-1}) + B(z^{-1})R(z^{-1}) + C(z^{-1})T(z^{-1}) \\ (15)$$

A. The Model of Superheated Steam Object
This passage is based on the superheated steam system of

$T(z^{-1})$
assignment.

is the expected characteristic polynomial

Anhui power station #2 boiler (600MW subcritical boiler). The main control system of steam temperature adopts cascade control system. The outer loop uses PID controller,

and the inner loop uses P controller. The structure is shown in transfer function of forward screen A is

Fig.1.

t_1

and

t_2

is the temperature transmitter slope

0.482

378°C . The transfer function of backward

coefficient. t_1 is the outlet temperature of desuperheater. t_2

$(1 - 27.74S)(1 - 28.65S)$

is the outlet temperature of superheater. The controlled object

screen is

0.576

$(1 - 155.59S)e$

$46S$. The parameter of inner PID K_p is

is composed of spray water adjusting valve, de-superheater and superheater. The degree of opening of the spray water

50. Thus we can get the main loop model

adjusting valve is the input signal of the control system, and the outlet temperature of the superheater is the output

3.75

(1□ 26.19S)(1□ 27.74S)(1□ 28.65S)(1□ 155.59S)

□ 98S

2

signal.

The controlled object consists of two parts.

- With the opening degree of the spray water adjusting valve as input signal, the desuperheater outlet temperature t_1 as output signal, this part is called leading segment.

- With the outlet temperature t_1 of desuperheater as the

This passage will use the superheated steam temperature model as the simulation research object. Superheater steam temperature control scheme in the paper adopts the cascade control system which combined outer master PID with pole assignment optimal prediction algorithm, it don't change the inner loop characteristics of the traditional cascade PID control system. The generalized controlled object model is as shown in Fig. 2. inputs signal, the outlet temperature t_2

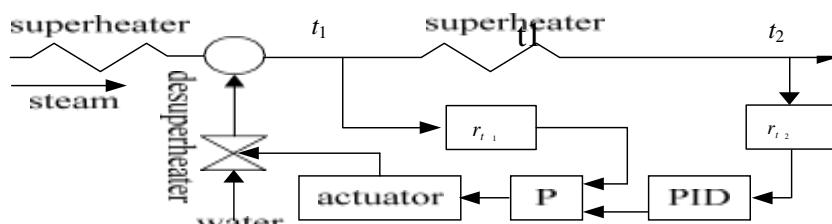


Fig.1.Steamtemperaturecascadecontrolsystem.

of superheater as

outputs signal. This part is called inert segment.

The boiler superheater steam temperature identification model with a load of 550MW is given in reference [6]. In which we choose the model of desuperheater A, forward screen, and backward screen as an example. The transfer function of primary desuperheater A is

0.270

(1□ 26.19S)

□ 15S. The

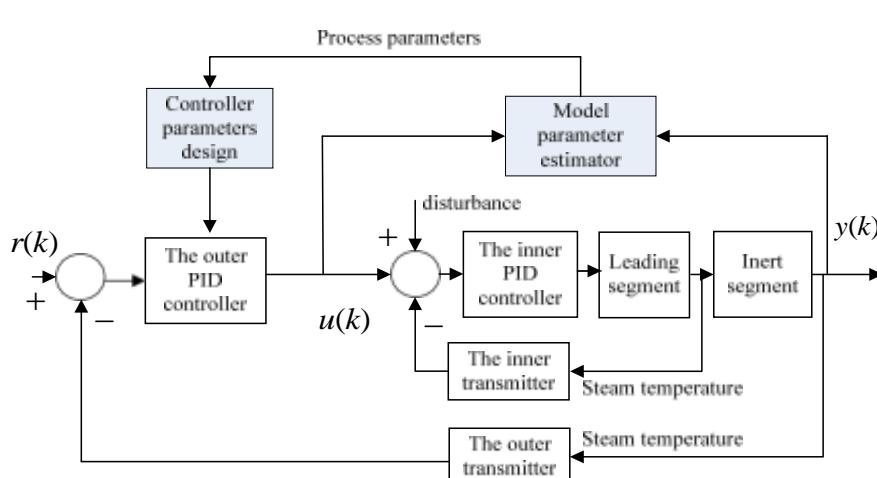


Fig.2.The structure of superheated steam temperature cascade system.

B.The Algorithm Flow BasedPoleAssignmentOptimalPrediction

The algorithm flow based pole assignment optimal prediction is shown in Fig. 3.

$$a_1 = 0.39, b = 2.28.$$

According to the viewpoint of pole placement, take the second-order system closed-loop transfer function standard form

C.Simulation Study

form

$$G_n(s) = \frac{n}{(s^2 + 2\zeta s + n^2)}$$

as the target. So the discrete characteristic polynomial is

In order to facilitate simulation, take the combination of the feedback close loop of leading segment and inertial segment

discrete characteristic polynomial is

$$T(z^{-1}) = 1 + 2e^{-nT} z^{-2}$$

as the generalized object, and adopt a sub-optimal reduction method [17] with time delay system to simplify the

$$T(z^{-1}) = \frac{1 + 2e^{-nT} z^{-2}}{\sqrt{1 - \xi^2}}$$

, n is undamped natural

generalized object. At the last we get the equivalent approximate model (typical first-order inertia object with pure time delay)

oscillation frequency, ω is damping ratio.

When $\omega = 0.707$ it is the optimal dynamic second-order response model. The principle of choosing polynomial

$$G(z) = \frac{3.75}{170S}$$

$$e^{-170S}$$

$$C(z^{-1})$$

is based on reference [16]. The shock which is

$$170.5S + 1$$

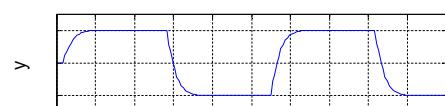
The parameters of discrete model to be identified are caused by mutations in the input side should be avoided.

Then we choose $C(z^{-1}) = 1 + 0.5z^{-1} + 0.1z^{-2}$.

The initial simulation parameters settings, the forgetting self-tuning PID controller has better dynamic and static characteristic than conventional PID controller. factor matrix

$$P = 0.95$$

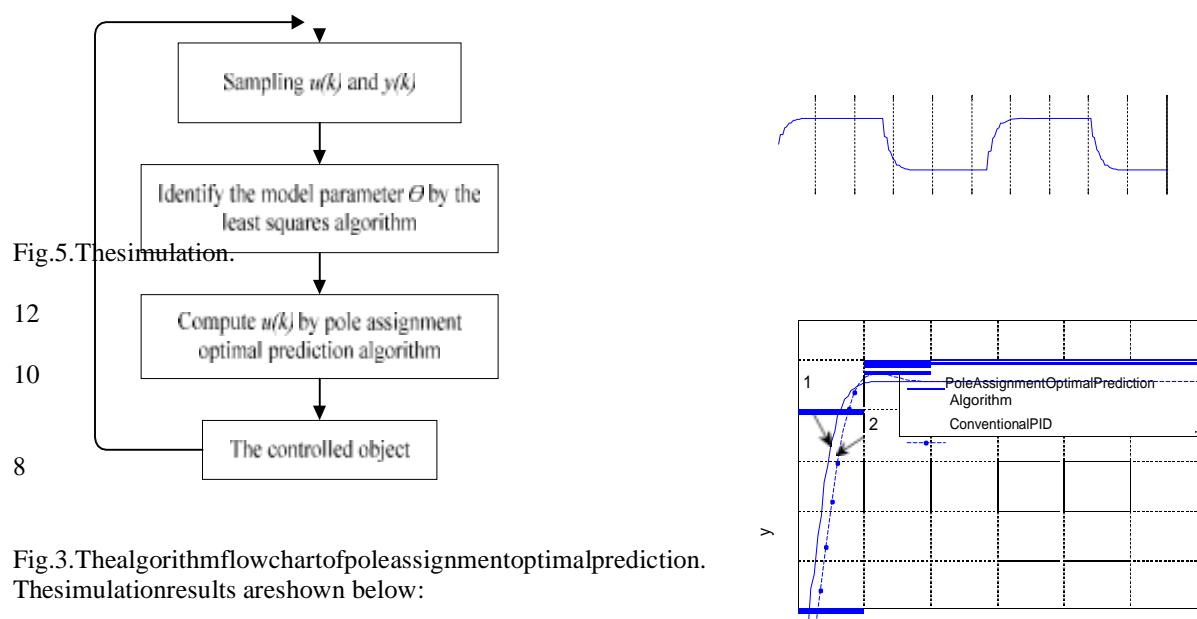
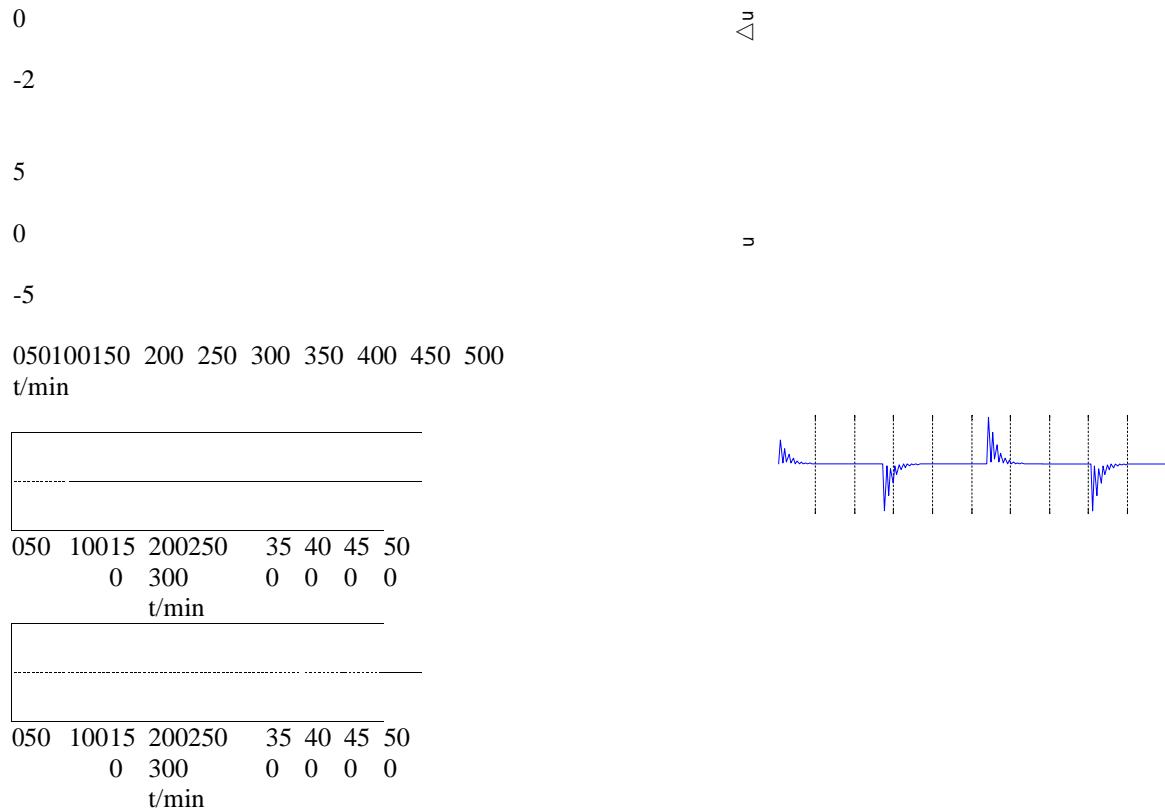
the estimation error covariance $P = 10I$ initial model parameters $P_0 = [ab]^T = [0.001 \ 0.001]^T$.



Initialization of model and control parameters

-10

2



2000 4000 6000 8000 10000 12000
t/s

Fig.6.Thecomparisonofsimulationcurves.

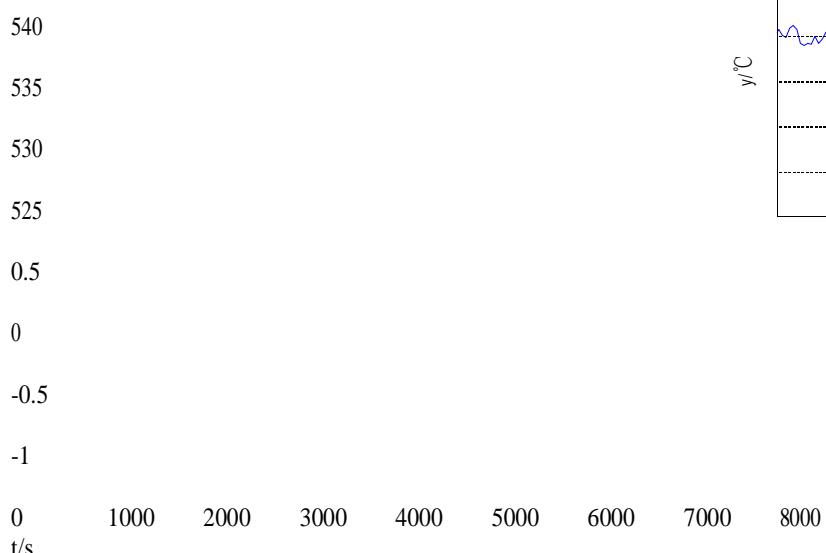
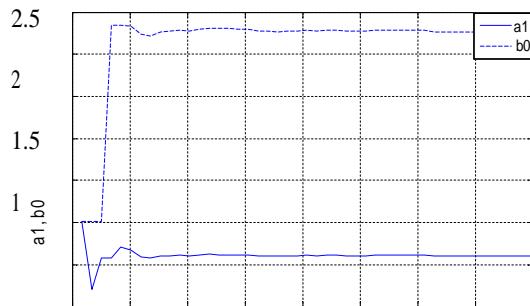


Fig.4.Modelparametersidentificationsimulation.

100 150 200 250 300 350 400
t/min

Fig.7.Steady-stateanddynamicsimulationresultofpoleassignmentoptimalpredictionalgorithm.

- Fig.7isthecurveofsimulatingtheactualboiler.On260minutes,10%disturbancewasaddedtothesystem

- Under the ideal conditions, the simulation curve of the boiler superheater with pole assignment optimal prediction algorithm is as shown in Fig. 5. We can see that the system has good response characteristics, such as fast adjustment speed, good following feature to input signal, effective in suppression of overshoot.
- From Fig. 6, curve 1 is the simulation result of adopting pole assignment optimal prediction algorithm. Curve 2 is the simulation result of adopting conventional PID. We can see that the rise time of curve 1 is less than the rise time of curve 2. There is almost no overshoot in curve 1. But for curve 2, there is about 8% overshoot. Therefore, the pole assignment optimal prediction load, we can see that the output temperature deviates from the set value at 5°C, and then return to the set temperature value about 540°C again. The result meets the actual production control requirement that the superheated steam temperature fluctuation range in dynamics situation is about $\pm 6^\circ\text{C}$, at steady-state condition is about $\pm 2^\circ\text{C}$.
- Fig. 8 is the simulation curve of adopting conventional PID controller. When disturbance was added to the system load, the output temperature deviates from the set value at 9°C , and then return to the set temperature value about 540°C. At steady-state condition, the superheated steam temperature fluctuation range is about $\pm 4^\circ\text{C}$. The control effect of adopting conventional PID controller is not ideal.

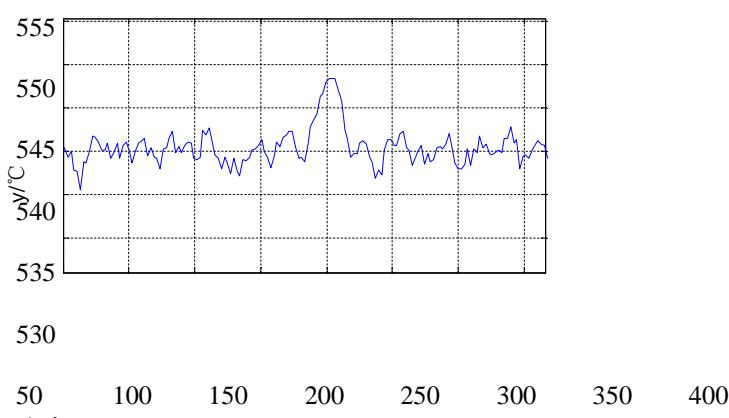


Fig.8.Steady-state and dynamic simulation result of conventional PID controller.

CONCLUSION

With more and more power boiler units develop to high capacity, multiple parameters, and high efficiency, the production system became increasingly complex. System coupling, time-variation, nonlinear become more prominent. The superheated temperature of the steam superheater is a typical control object of nonlinear, long-delay, and great inertia. Although there are many new control methods for power steam temperature, the PID algorithm is still widely used because of its simple control structure and algorithm, easy to implement, and good applicability. In this paper, the PID controller parameter tuning method based on pole assignment optimal prediction algorithm is proposed. The model of superheated steam temperature is also simulated in this passage. The result of simulation verifies the effectiveness of the pole assignment optimal prediction algorithm.

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